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Dewald

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(54) **ILLUMINATION SYSTEM FOR SCROLLING COLOR RECYCLING**

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U.S. patent application Ser. No. 09/705,467, Dewald et al.,
filed Nov. 3, 2000.

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patent is extended or adjusted under 35
U.S.C. 154(b) by 0 days.

* cited by examiner

(21) Appl. No.: **10/028,023**

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(22) Filed: **Dec. 21, 2001**

(57) **ABSTRACT**

(65) **Prior Publication Data**

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Related U.S. Application Data

(60) Provisional application No. 60/258,985, filed on Dec. 29,
2000.

Distortion optics are used to efficiently couple a spiral color
wheel and an orthogonal modulator. Light **602** from a light
source enters an aperture in a reflective end of a recycling
integrator rod **604**. The light travels through the rod and exits
the end of the rod adjacent a sequential color filter **606**,
shown as a spiral color wheel. The shape of the light beam
608 exiting the integrator rod **604** is determined by the shape
of the exit aperture of the integrating rod **606**. The exit
aperture of the integrating rod **606** typically is formed by a
reflective exit aperture on the exit face. A cross section of the
light beam **608** exiting the sequential color filter includes
several bands of filtered light, one for each of the filter
segments of the color wheel illuminated by the light beam.
The curvature of the color bands makes it difficult for a row
addressed spatial light modulator to efficiently use the light.
Illumination system **600** eliminates or mitigates this prob-
lem by distorting the light from the integrating rod to
straighten the curved borders between the adjacent filter
segments. The light **608** from the sequential color filter **606**
is distorted by distortion optics **610**, **612** to make the
boundaries between the white or primary colored light
segments align with the rows of the spatial light modulator
614.

(51) **Int. Cl.**⁷ **G06K 9/40**; H04N 9/12;
G03B 21/00

(52) **U.S. Cl.** **382/274**; 348/742; 353/31

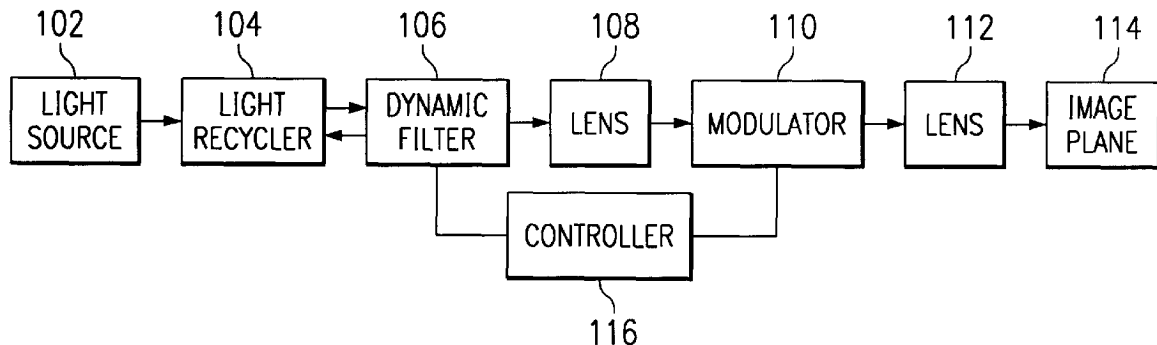
(58) **Field of Search** 359/631, 626,
359/636, 291, 889, 237; 353/31, 84, 94,
98, 34, 70, 101; 345/46, 83, 204; 348/742,
751, 744; 382/274

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50 Claims, 5 Drawing Sheets



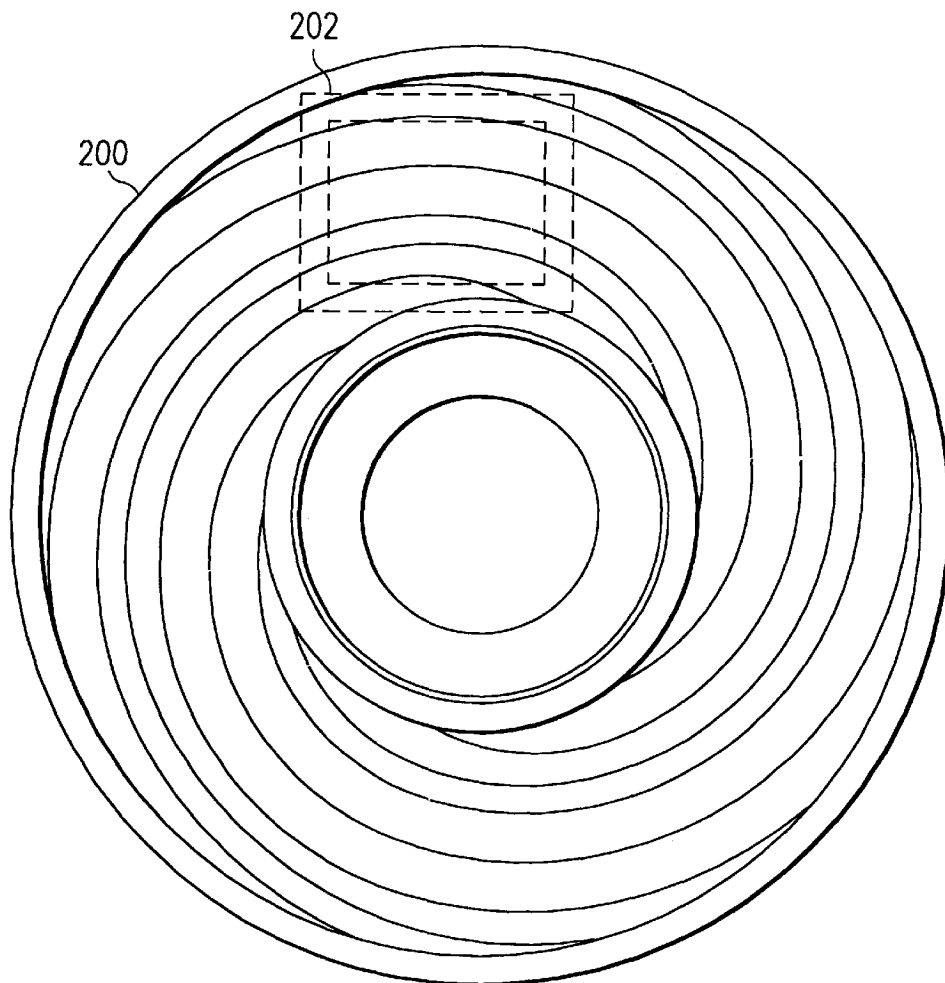
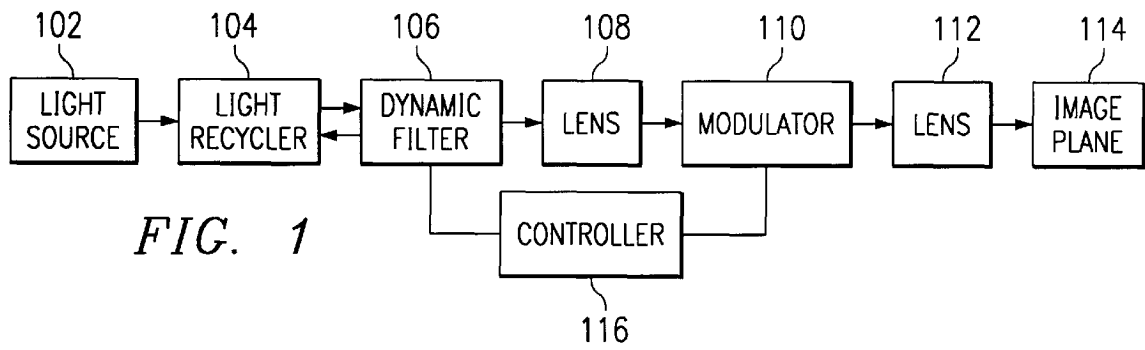


FIG. 2

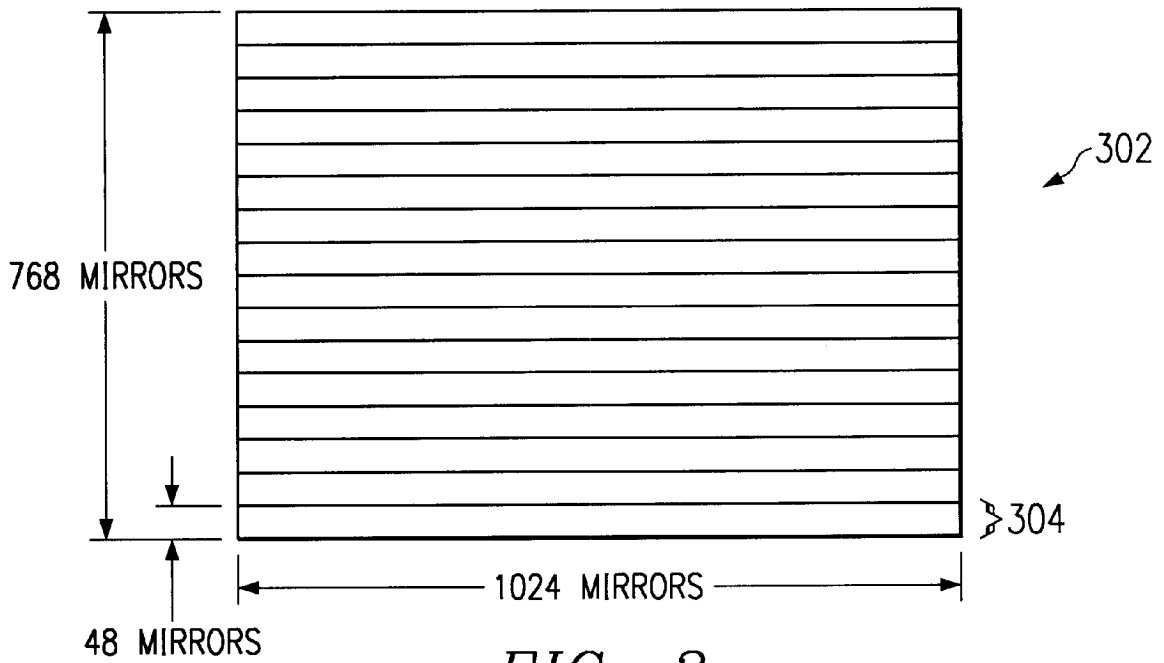


FIG. 3

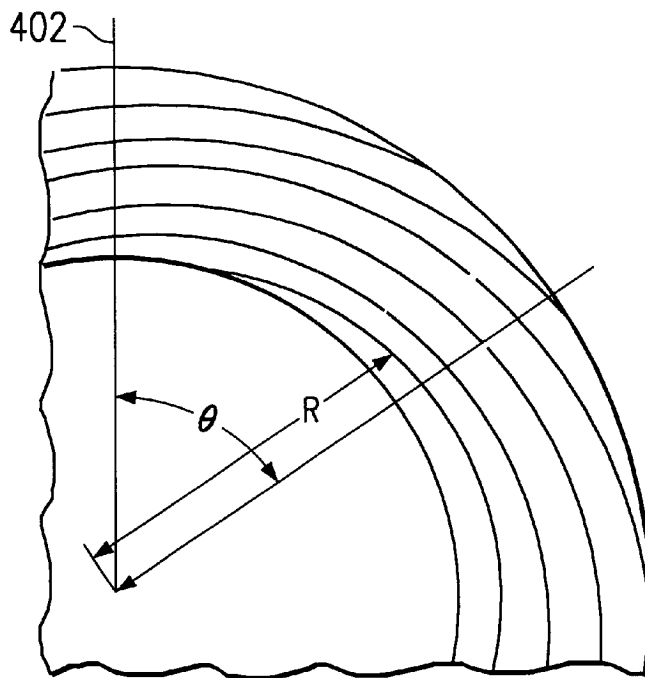
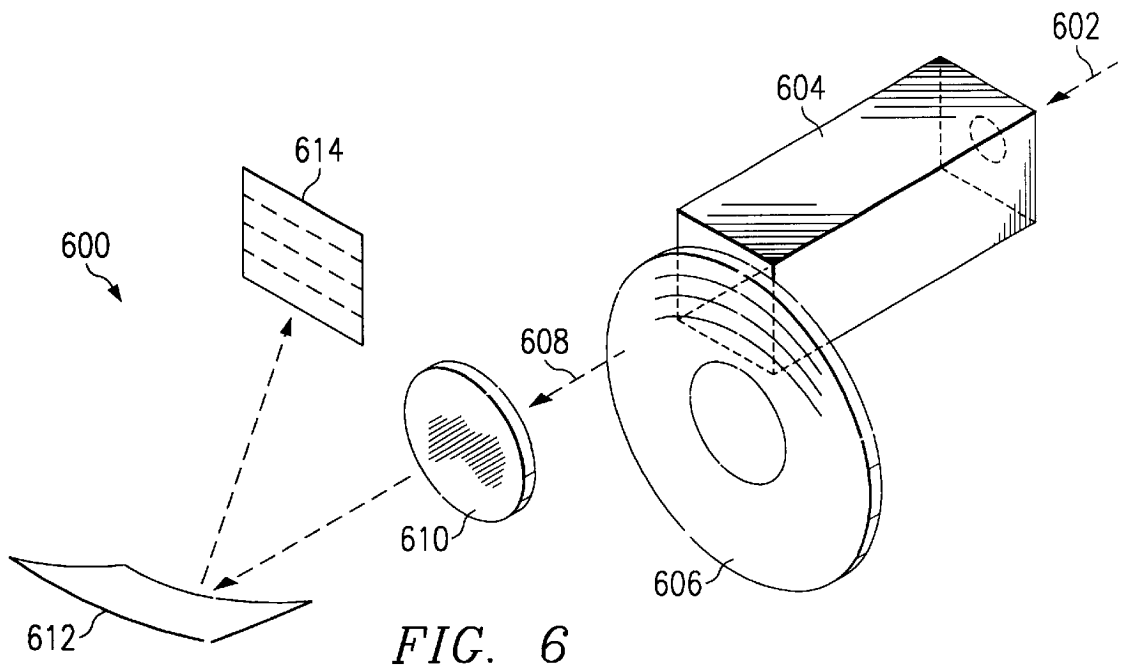
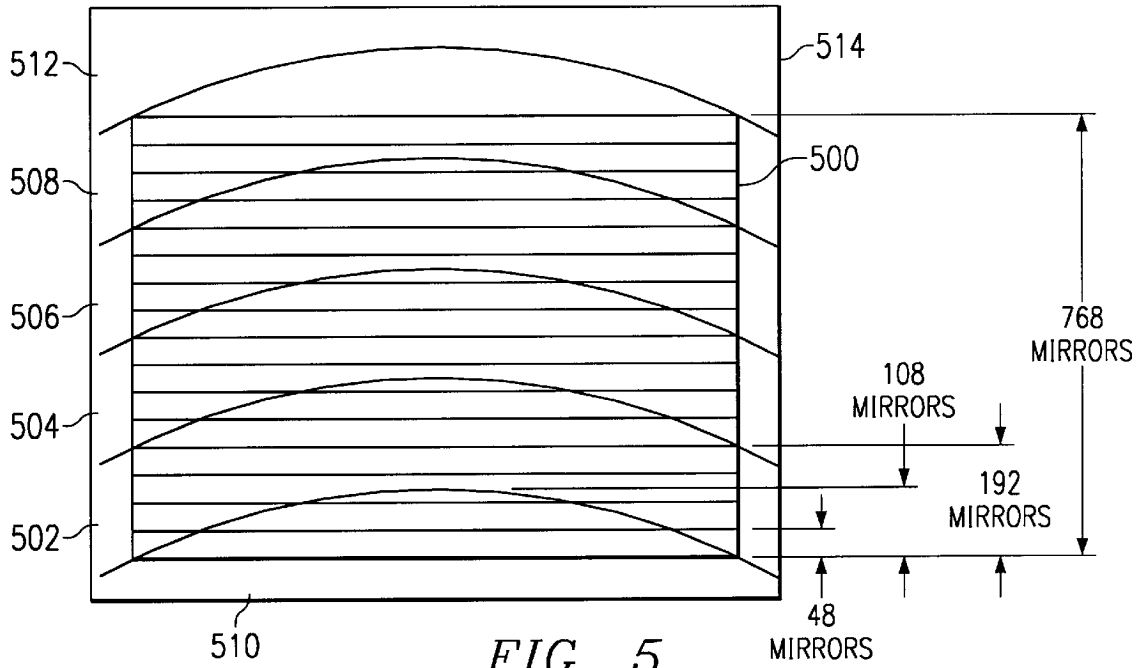


FIG. 4



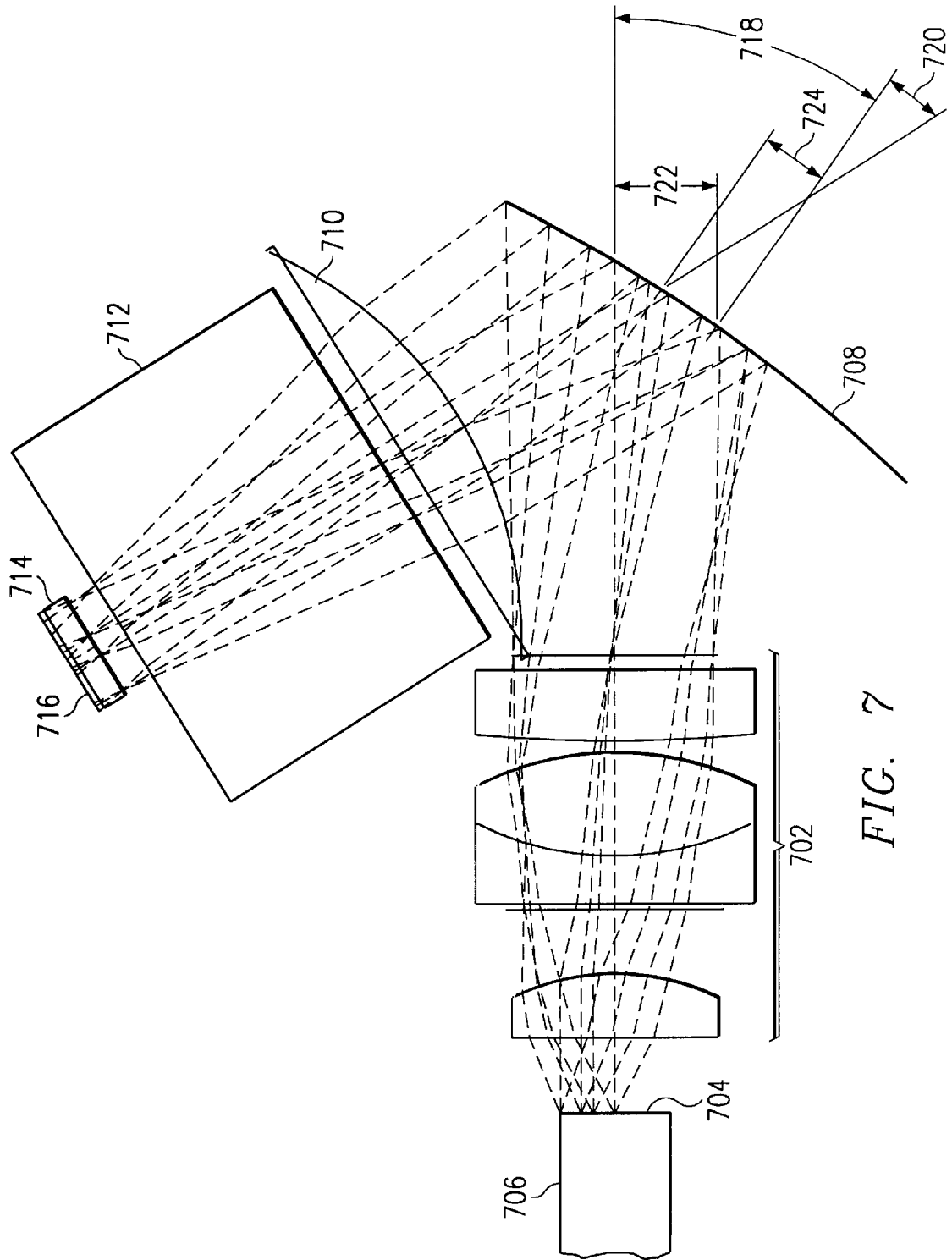
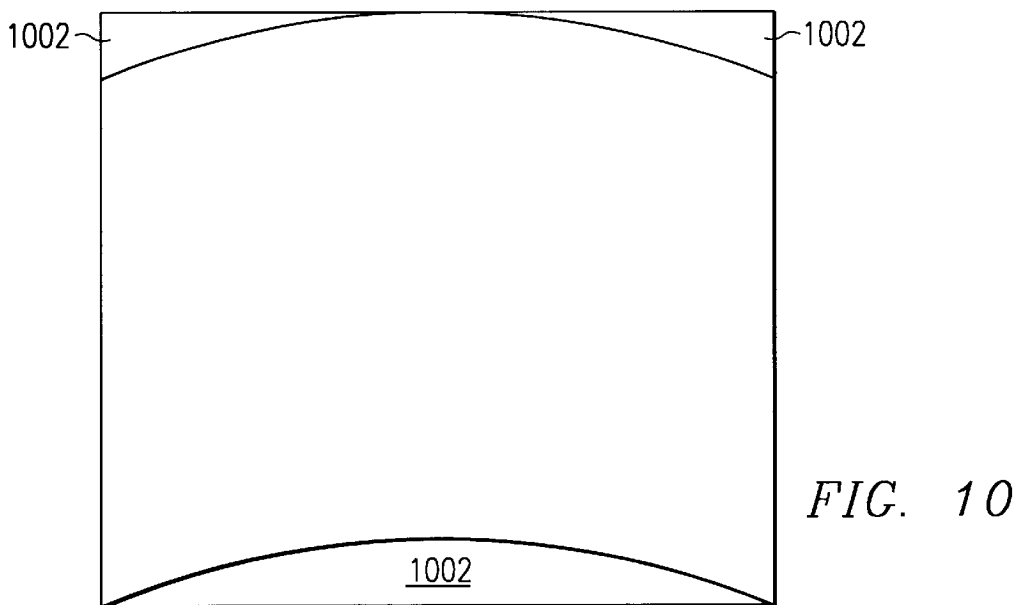
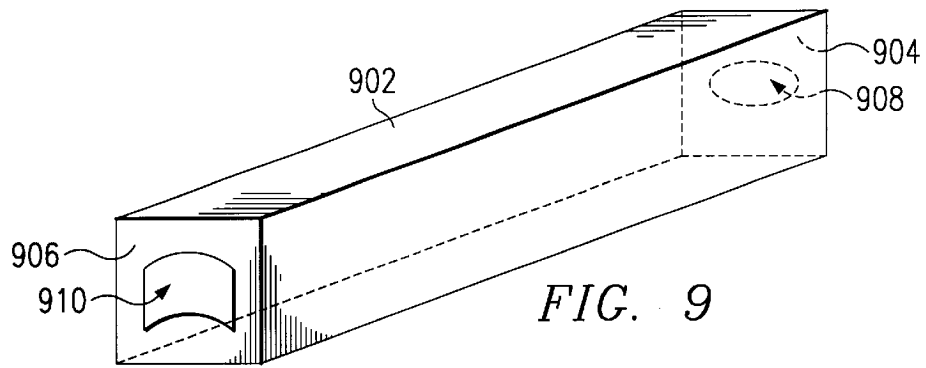
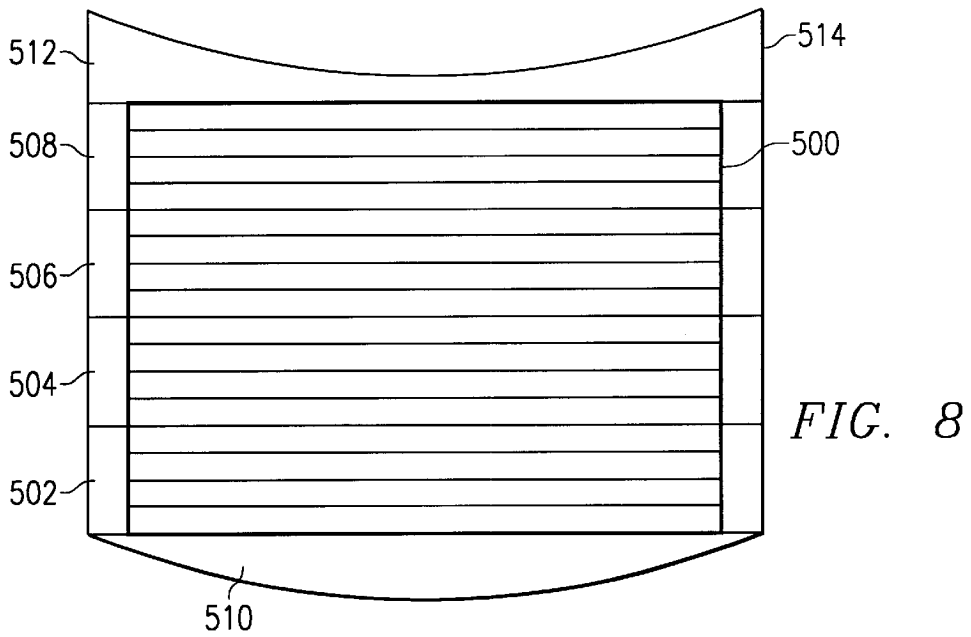


FIG. 7



**ILLUMINATION SYSTEM FOR SCROLLING
COLOR RECYCLING**

**CROSS-REFERENCE TO RELATED
APPLICATIONS**

This application claims priority under 35 USC §119(e)(1) of provisional application No. 60/258,985 filed Dec. 29, 2000.

The following patents and/or commonly assigned patent applications are hereby incorporated herein by reference:

Patent No.	Filing Date	Issue Date	Title
6324006	May 17, 2000		Spoke Light Recapture In Sequential Color Imaging Systems
09/705,467	Nov. 3, 2000		Sequential Color Recapture for Projection Systems

1. Field of the Invention

This invention relates to the field of display systems, more particularly to scrolling color recapture projection display systems.

2. Background of the Invention

Viewers evaluate display systems based on many criteria such as image size, resolution, contrast ratio, color purity, and brightness. Image brightness is a particularly important metric in many display markets since the available brightness can limit the image size of a projected image and controls how well the image can be seen in venues having high levels of ambient light.

Projection display designers increase the brightness of a given projection display by increasing the light source used to form the image. Increasing the light source, however, also increases the cost, size, and weight of the display system. Additionally, larger light sources generate additional heat that must be dissipated by the display.

Many other factors affect the brightness of the images produced by the display system. One of the major factors is the number of modulators used to modulate the light used to produce the image. Display systems that use a modulator with a very fast response time, such as the Digital Micromirror Device™, can use a single modulator to create a full color image. Other display systems use three modulators, such as liquid crystal display (LCD) panels or micromirrors, to create a full color image.

Micromirror-based display systems typically operate the micromirrors in a digital, or bistable, manner. Digital operation fully deflects a given micromirror to either a first position or a second position. The illumination optics of the display device illuminate the entire array of micromirror cells. Micromirrors deflected to the first position reflect light along a first path, whereas micromirrors deflected to a second position reflect light along a second path. The projection optics of the display system collects the light from the mirrors in the first position and focus the light onto an image plane. The light reflected by mirrors in the second position is prevented from reaching the image plane. An image pixel associated with a mirror in the first position is brightly illuminated, whereas an image pixel associated with mirrors in the second position are not illuminated.

Pulse width modulation creates the perception of gray scale intensities with a digital micromirror device or other spatial light modulator. When using pulse width modulation,

a given micromirror element is rapidly turned on and off in response to a digital intensity word. The duty cycle of the mirror determines the total amount of light contributed to an image pixel. If the pixel is pulsed quickly enough, the human eye will accurately measure the average intensity of the pixel, but will fail to detect the pulsing.

Full-color images also are produced by taking advantage of the relatively slow response time of the human eye. Each frame period is divided into at least three periods. During each period, a primary color image is produced. If the primary color images are produced in rapid succession, the eye will perceive a single full-color-image.

An alternative to the sequential color display system is a three-modulator display system. The three-modulator display system is very similar to the sequential color display system in that they both form full color images by the combining three primary color images. The disadvantage of the three-modulator display system is the cost of the three modulators and the complex optics required both to split the white light beam from the light source into three primary color light beams and to recombine the modulated primary color light beams.

The disadvantage of the single-modulator sequential color display systems is its low image brightness. Because the white light source is time-divided into three primary color light beams, most of the light at any given time is not used. For example, when the blue primary color image is being formed, the green and red output of the white light source are filtered out of the light beam. Thus, a sequential color display system, while generally less expensive than the three-modulator display system, makes very inefficient use of the light produced by the light source.

The lost light not only reduces the brightness of the image produced by the display system, discarding the light creates several problems for the display system. The light filtered out of the light beam generally becomes stray light that the display system must control to prevent from reaching the image plane and degrading the contrast of the displayed image. The off-primary light is generally converted to heat. The heat must be dissipated by using larger fans, which in turn increase the noise produced by the display system and increase the size of the display system.

A recently developed projector architecture, commonly called sequential color recapture or scrolling color recycling (SCR), uses a sequential color filter with filter segments small enough that at least one of each primary color, and white if used, are simultaneously imaged on the modulator. The light rejected by the filter is reflected and presented to the filter a second time, hopefully to another filter segment. Assuming the recycling mechanism is perfectly efficient, the system has the effect of directing all of the light of each primary color to the corresponding primary color filter and is therefore potentially as bright as a three modulator system. Considering the inefficiencies involved the system is 1.5 to 1.8 times as bright as a comparable one modulator system.

The SCR illumination system is difficult to use with conventional micromirror devices. Conventional micromirror devices group many rows together in a reset group and apply the same reset bias voltage to the entire group. Since many entire rows must be reset simultaneously, it is difficult to track the shadow of the filter boundary across the face of the modulator. What is needed is a system and method to allow efficient use of an SCR illumination system with a block reset device such as a micromirror.

SUMMARY OF THE INVENTION

Objects and advantages will be obvious, and will in part appear hereinafter and will be accomplished by the present invention which provides a method and system for efficient scrolling color recycling with a line-addressed modulator. One embodiment of the claimed invention provides a display system. The display system comprising: a light source, a recycling integrator rod, a sequential color filter a spatial light modulator, distortion optics, and a controller. The light source produces producing a beam of white light along a path. The sequential color filter receives the beam of white light to form a filtered beam of light having a first cross section. The spatial light modulator has a second cross section. The distortion optics on an optical path between the sequential color filter and the spatial light modulator. The distortion optics operable to receive and distort the filtered beam of light to form a filtered beam of light having a second cross section. The controller is electrically connected to the spatial light modulator for providing image data to the spatial light modulator. The spatial light modulator being operable to modulate the filtered beam according to the image data.

Another embodiment of the claimed invention provides a display system. The display system comprising: a light source, a sequential color filter a spatial light modulator, distortion optics, and a controller. The light source produces producing a beam of white light along a path. The sequential color filter comprising a spiral color wheel. The sequential color filter receives the beam of white light to form a filtered beam of light having a first cross section. The first cross section having at least one curved side following a boundary between two segments on the spiral color wheel. The spatial light modulator has a second cross section. The distortion optics on an optical path between the sequential color filter and the spatial light modulator. The distortion optics operable to receive and distort the filtered beam of light to form a filtered beam of light having a second cross section. The controller is electrically connected to the spatial light modulator for providing image data to the spatial light modulator. The spatial light modulator being operable to modulate the filtered beam according to the image data.

Another embodiment of the present invention provides a method of illuminating a spatial light modulator. The method comprising: producing a beam of white light along a path; sequentially color filtering the beam of white light to form a filtered beam of light having a first cross section; distorting the filtered beam of light to have a second cross section; and spatially modulating the distorted beam of light using a spatial light modulator, the distorting operable to improve the alignment of filter boundaries to groups of spatial light modular elements.

Another embodiment of the present invention provides a method of illuminating a spatial light modulator. The method comprising: producing a beam of white light along a path; sequentially color filtering the beam of white light using a spiral color wheel to form a filtered beam of light having a first cross section, the first cross section having at least one curved side following a boundary between two segments on the spiral color wheel; recycling light rejected by the color filtering using a recycling integrator on the path of the white light beam, the recycling integrator having an exit aperture defining the first cross section; distorting the filtered beam of light to have a second cross section; and spatially modulating the distorted beam of light using a spatial light modulator, the distorting operable to improve the alignment of filter boundaries to groups of spatial light modular elements.

BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present invention, and the advantages thereof, reference is now made to the following descriptions taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a block diagram of a sequential color recycling system according to one embodiment of the present invention.

FIG. 2 is a plan view of a spiral color wheel according to one embodiment of the disclosed invention.

FIG. 3 is a plan view of a micromirror array showing the arrangement of the micromirrors into groups of rows.

FIG. 4 is a plan view of a portion of a spiral color wheel detailing the curvature of the filter segments.

FIG. 5 is a plan view of a spatial light modulator showing the alignment of the filtered light beam on the face of the spatial light modulator.

FIG. 6 is a perspective view of one embodiment of the present invention using distortion optics to efficiently couple a spiral color wheel and an orthogonal modulator with the modulator elements organized in groups of rows.

FIG. 7 is a plan view of one embodiment of an illumination optical system for the display system of FIG. 6.

FIG. 8 is a plan view of the surface of the spatial light modulator of FIG. 5 illuminated by a light beam after the light beam has been distorted by the distortion optics of FIG. 6.

FIG. 9 is a perspective view of an integrating rod that includes a mirrored entrance face and an optional exit face aperture.

FIG. 10 is a plan view of the exit aperture of the integrating rod of FIG. 9 according to one embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

A new optical system and method has been developed that enables the efficient use of scrolling color recycling illumination with line addressed modulators. The new system and method distort the image of the color wheel that is projected onto the face of the spatial light modulator to optically straighten the boundaries between the curved color filter segments. This enables efficient use of row addressed modulators since an entire row is illuminated by a single color and the illumination color for all the elements in a row changes at the same time.

FIG. 1 is a block diagram of a sequential color recycling system according to one embodiment of the present invention. In FIG. 1, light source 102 provides a beam of light to a light recycler 104. The light recycler 104, which sometimes includes the lamp housing or reflector, homogenizes the beam of light and passes it to a dynamic filter 106. The dynamic filter is typically a set of moving dichroic filters, such as a color wheel. Each filter in the dynamic filter has a pass band in which light of a range of wavelengths is selected, in this case transmitted, while out of band light is rejected, in this case reflected.

Light transmitted by the dynamic filter 106 is focused by lens 108 onto a spatial light modulator 110. The spatial light modulator 110 modulates the light to form an image bearing beam of light that is focused by lens 112 onto an image plane 114. Controller 116 receives image data and sends primary color image data to the modulator 110 in synchronization with the dynamic filter 106.

As described above, the dynamic filter transmits light in its pass band and rejects light outside its pass band. FIG. 1 shows the rejection path leading back to the light recycler 104. The light recycler 104 receives the rejected light and reflects it back to the dynamic filter 106. If the recycled light strikes a filter having a different pass band it may be transmitted to lens 108. Rejected portions of the recycled light are again recycled by the light recycler 104 and presented to the dynamic filter 106. This process continues until the light either is absorbed by the light recycler 104, accepted by the dynamic filter 106, or escapes the light recycler 104.

One element of the system shown in FIG. 1 is the dynamic filter 106. The dynamic filter must provide one or more segments of each primary color filter to the light beam at all times in order for all of the recycled light to be able to find a filter through which it may pass. Although the filters for each color need not be the same size, if the recycling operation is efficient there is no advantage to unequal sized filters.

FIG. 2 is a plan view of one embodiment of multi-segment spiral color wheel. The color wheel 200 of FIG. 2 has two sets of four color filters. Each set includes one of each of the primary colors, and a clear or white segment that allows all visible light to pass through it. Each primary colored segment transmits one of the primary colors and rejects the other two primary colors. The color wheel of FIG. 2 is 35 mm in diameter and has 2 sets of primary filters, typically red, green, and blue, plus two clear segments, for a total of 10 filter segments.

FIG. 2 shows the outline of the light beam 202 that passes through the color wheel. The outline of the light beam 202 is determined by the shape and location of the integrating rod. The integrator rod is typically positioned very close to the color wheel to ensure that light reflected by the color wheel is recaptured by the integrating rod. Light from the color wheel is imaged onto the spatial light modulator such that a separate portion of the spatial light modulator is illuminated by each filter.

The spiral color wheel of FIG. 2 is used to reduce the size of the color wheel while maintaining good alignment between the modulator and the illuminated segments of the color wheel. The spiral color wheel shown in FIG. 2 has color filters whose boundaries form the "spiral of Archimedes." The spiral of Archimedes is defined by:

$$r=a\theta$$

where r is the radius or distance of said interface from said center, a is a constant, and θ defines an arc between said interface and a reference. A different reference is used for each boundary between two filters.

A typical micromirror device 302 is shown in FIG. 3. The micromirror shown contains 768 rows of mirrors, with 1024 mirrors in each row. The typical micromirror device has sixteen reset groups 304 of mirrors. Each mirror in the reset group is electrically connected and receives the same mirror bias signal. The mirror bias signal determines when the mirror assumes the position dictated by the memory cell underlying the mirror, and when the mirror is reset to a neutral position. The micromirror reset groups 304 typically are adjacent rows of mirrors. For example, a 1024×768 micromirror array includes 16 groups of 48 rows, each row has 1024 mirrors. Each reset group then consists of 49,152 mirrors.

Since the modulator is typically arranged in horizontal rows of modulator cells that receive many of the same

operating signals and bias voltages, the operation of the modulator is more efficient when the primary color segments have horizontal boundaries and move vertically from row to row. The modulator elements can also be arranged in vertical groups of columns, in which case the primary color segments should have vertical boundaries and move horizontally from column to column.

FIG. 4 shows the relationship between the reference 402, θ , and the radius r . The result of using the spiral of Archimedes is that each boundary approximates an inclined plane sliding past the light valve. The boundary is not straight, so it cannot be parallel to the rows of modulator elements. The boundary does, however, form curve that is tangential to the rows of the modulator elements and the boundary maintains the same curve and speed across the entire face of the modulator, even when using a small filter wheel.

The spirals are designed and aligned to the spatial light modulator such that the tangent of the boundaries between adjacent segments is approximately horizontal to the rows of spatial light modulator. As the spiral wheel turns, the portion of the spiral passing through the beam of light shifts along the spiral maintaining good alignment between the segments and the modulator.

As the color wheel turns, the three primary color segments imaged onto the spatial light modulator move across the face of the spatial light modulator. FIG. 5 shows the image of a red 502, blue 504, green 506, and two clear 508, 510 segments moving across the face of a spatial light modulator 500. As the second clear segment 508 moves onto the spatial light modulator 500 from the top, the first clear segment 510 moves off the modulator to the bottom. A second red segment 512 is moving toward the modulator, but has not reached it in FIG. 5.

Since each color appears on a different region of the modulator at any given time, the image data provided to the modulator is a mixture of data for all three primary colors and the white segment. For example, while one region of the modulator is operated using red data, other regions of the modulator are operated using green and blue data. During periods in which a boundary between two regions sweeps across a row, image data representing the white content of the image is driven to the mirrors in the row. The net effect of driving the row with white data during every transition of the color wheel is the primary colors are summed to create white and the potential brightness of the display is raised.

As shown in FIG. 5, each boundary between two adjacent color filters may be imaged over 108 rows of modulator elements. Therefore, at any time 432 of the 768 modulator rows are illuminated by light of two colors and are driven with the white data. The lack of time during which the rows can be driven with pure primary colored light reduces the color saturation achievable by the display system. Smaller color wheels, which enable smaller projectors and are therefore more desirable, increase the curvature of the boundaries between the filter segments and further reduce the saturation of the projected images.

A solution to this problem is to introduce distortion to the image of the color filter projected onto the micromirror device. FIG. 6 is a simplified perspective view of one embodiment of the present invention using distortion optics to efficiently couple a spiral color wheel and an orthogonal modulator. In FIG. 6, light 602 from a light source enters an aperture in a reflective end of a recycling integrator rod 604. The light travels through the rod, reflecting on the surfaces of the rod—whether by internal reflection in a solid rod or by mirrored surfaces on a hollow or solid rod—and exits the

end of the rod adjacent a sequential color filter **606**, in this case a spiral color wheel.

The shape of the light beam **608** exiting the integrator rod **604** is determined by the shape of the exit aperture of the integrating rod **606**. The exit aperture of the integrating rod **606** of prior art systems typically is the entire exit face of a rectangular integrating rod **606** with an aspect ratio equal to the aspect ratio of the spatial light modulator. For reasons that will become obvious, the present invention typically changes the aspect ratio of the rod and optionally includes a reflective exit aperture on the exit face.

A cross section of the light beam **608** exiting the sequential color filter is shown as rectangle **514** of FIG. **5**. The rectangle shape of the light beam includes several bands of filtered light, one for each of the filter segments of the color wheel illuminated by the light beam. As described above, the curvature of the color bands makes it difficult for a row addressed spatial light modulator to efficiently use the light. The new illumination system eliminates or mitigates this problem by distorting the light from the integrating rod to straighten the curved borders between the adjacent filter segments.

In FIG. **6**, the light **608** from the sequential color filter **606** is distorted by distortion optics **610**, **612** to make the boundaries between the white or primary colored light segments align with the rows of the spatial light modulator **614**. In general, any type of distortion optic may be used including, for purposes of illustration and not for purposes of limitation, single and multiple component spherical or aspherical lenses, and spherical or aspherical mirrors. Mirrors may provide the advantage of not introducing chromatic aberrations. Typically, the distortion optics are mounted off-axis to assist in distorting the shapes of the color filters. In FIG. **6**, the distortion optics include both a lens system **610** and a curved mirror **612**.

FIG. **7** is a plan view of one embodiment of an illumination optical system for the display system of FIG. **6**. In FIG. **7**, a condenser lens group **702** gathers and collimates the light leaving the exit face **704** of an integrating rod **706**. The light leaving the collimating group is reflected by a conic mirror **708**. The conic mirror **708** reflects the light to a collecting lens **710** that passes the light to a TIR prism assembly **712**. After passing through the TIR prism assembly **712**, the light passes through the micromirror package window **714** before reaching the micromirror **716**.

The conic mirror **708** is positioned at an angle **718** to the axis of the condenser optics **702** and an angle **720** to the axis of the collecting lens **710**. Additionally, the center of the aspherical mirror **708** is offset **722** from the intersection of the axis of the condenser optics **702** and offset **724** from the intersection of the axis of the collecting lens **710**.

Depending on the distortion required, the mirror could be spherical, conical, or aspherical. For the embodiment shown in FIG. **7**, the conic mirror is described by:

$$z = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}}$$

where: c is the curvature, r is the radial coordinate in lens units, and k is the conic constant. As shown in Table 1, the curvature of the mirror **708** is -200 . The conic constant of the mirror **708** is 10 . The conic constant is less than -1 for hyperbolas, -1 for parabolas, between -1 and 0 for ellipses, 0 for spheres, and greater than 0 for oblate ellipsoids.

For the embodiment of FIG. **7**, the offset **722** from the axis of the condenser optics **702** is 14.704516 mm. The angle between the mirror **708** and the axis of the condenser optics

702 is 35 degrees. The offset **724** from the axis of the collecting lens **710** is 0.7545004 mm. The angle between the mirror **708** and the axis of the collecting lens **710** is 23 degrees. Other embodiments use different mirrors or lenses in place of the aspherical mirror **708**. Table 1 is a complete listing of the optical system shown in FIG. **7**.

FIG. **8** is a plan view of the surface of the spatial light modulator **500** illuminated by the light beam **514** after the light beam has been distorted by the distortion optics of FIG. **6**. In FIG. **8**, the boundaries between the filter segments have been straightened by the distortion optics to align with the rows of the spatial light modulator **500**. The distortion optics need not perfectly align the boundaries between the various colors with the modulator rows, but the better the alignment the better the efficiency.

As shown in FIGS. **5** and **8**, the curved filter segments require a rectangular light beam to be much larger than the rectangular modulator on which its distorted image will be focused. This reduces the intensity of the light actually focused onto the modulator. A scrolling color recycling system can recover this excess light by using a reflective aperture that masks the exit end of the integrating rod except for the portion of the rod that actually is imaged onto the modulator.

FIG. **9** is a perspective view of an integrating rod **902** that includes a mirrored entrance face **904** and an optional exit face **906** aperture **910**. The exit face **906** typically is mirrored. The importance of the mirrored aperture on the exit face **906** increases as the curve of the spiral color filters increases. The open entrance aperture **908** on the entrance face **904** is shaped and sized to efficiently couple the light from a light source into the integrating rod **902**. An open exit aperture **910** on the exit face **906** of the integrating rod **902** is shaped and sized to be imaged onto the face of the spatial light modulator without excess overflow.

In FIG. **9**, light traveling through the integrator rod **902** that strikes the mirrored portion of the exit face is reflected back through the integrating rod **902** to the entrance face **904**. If the returning light strikes the mirrored portion of the entrance face **904** it reflects back through the integrating rod **902** and has another opportunity to pass through the exit aperture **910**. Light continues to reflect inside the integrating rod **902** until it passes through either of the apertures or is absorbed.

FIG. **10** is a plan view of the exit aperture of the integrating rod according to one embodiment of the present invention. In FIG. **10**, the aperture extends to all four sides of the integrating rod. Three mirrored areas **1002** define a clear aperture with two curved sides that match the curve of the filter segments as they pass by each side of the integrating rod. The size of the open aperture allows light from the integrating rod to illuminate one full segment of each segment color on the color wheel.

Thus, although there has been disclosed to this point a particular embodiment for an efficient illumination system for a scrolling color recycling projection system and method therefore, it is not intended that such specific references be considered as limitations upon the scope of this invention except insofar as set forth in the following claims. Furthermore, having described the invention in connection with certain specific embodiments thereof, it is to be understood that further modifications may now suggest themselves to those skilled in the art, it is intended to cover all such modifications as fall within the scope of the appended claims. In the following claims, only elements denoted by the words "means for" are intended to be interpreted as means plus function claims under 35 U.S.C. §112, paragraph six.

TABLE 1

LENS DATA				
GENERAL LENS DATA:				
Surfaces	23			
Stop	1			
System Aperture	Object Space NA = 0.47			
Glass Catalogs	OHARA minolta			
Ray Aiming	Real Reference, Cache On			
X Pupil shift	0			
Y Pupil shift	0			
Z Pupil shift	0			
Apodization	Gaussian, factor = 6.00000E-001			
Effective Focal Length	-76.47616 (in air)			
Effective Focal Length	-76.47616 (in image space)			
Back Focal Length	146.8078			
Total Track	3120.381			
Image Space F/#	0.02393721			
Paraxial Working F/#	1.748671			
Working F/#	1.874482			
Image Space NA	0.2749141			
Object Space NA	0.47			
Stop Radius	-1597.432			
Paraxial Image Height	11.91844			
Paraxial Magnification	-1.862256			
Entrance Pupil Diameter	-3194.865			
Entrance Pupil Position	0			
Exit Pupil Diameter	82.574			
Exit Pupil Position	-148.2844			
Field Type	Object height in Millimeters			
Maximum Field	6.4			
Primary Wave	0.55			
Lens Units	Millimeters			
Angular Magnification	-38.69093			
Fields: 4				
Field Type: Object height in Millimeters				
#	X-Value	Y-Value	Weight	
1	0.000000	0.000000	1.000000	
2	0.000000	2.500000	1.000000	
3	0.000000	4.000000	1.000000	
4	0.000000	6.400000	1.000000	
Vignetting Factors				
#	VDX	VDY	VCX	VCY
1	0.000000	0.000000	0.000000	0.000000
2	0.000000	0.000000	0.000000	0.000000
3	0.000000	0.000000	0.000000	0.200000
4	0.000000	0.000000	0.100000	0.300000
Wavelengths: 5				
Units: Microns				
#	Value	Weight		
1	0.450000	1.000000		
2	0.490000	1.000000		
3	0.550000	1.000000		
4	0.610000	1.000000		
5	0.650000	1.000000		
SURFACE DATA SUMMARY:				
Surf	Type	Radius	Thickness	
OBJ	STANDARD	Infinity	-3000	
STO	STANDARD	Infinity	3000	
2	STANDARD	Infinity	9	
3	STANDARD	-383.7957	7	
4	STANDARD	-29.16254	8	
5	STANDARD	Infinity	0.467447	
6	STANDARD	-1641.567	6	
7	STANDARD	42.75783	12	
8	STANDARD	-31.89381	1	
9	STANDARD	200	8	

TABLE 1-continued

LENS DATA				
5	10	STANDARD	1233.289	1.913955
	11	STANDARD	Infinity	47
	12	COORDBRK	—	0
	13	COORDBRK	—	0
	14	STANDARD	-200	20
	15	COORDBRK	—	0
	16	COORDBRK	—	-50
	17	STANDARD	-46.57814	-8
	18	STANDARD	Infinity	-2
	19	STANDARD	Infinity	-36.3
	20	STANDARD	Infinity	-4
	21	STANDARD	Infinity	-3.08
	22	STANDARD	Infinity	-0.5
	IMA	STANDARD	Infinity	
SURFACE DATA DETAIL:				
	Surf	Glass	Diameter	Conic
	OBJ		12.8	0
	STO		3194.865	0
	2		12.8	0
	3	S-LAH79	24	0
	4		24	0
	5		21.39037	0
	6	SF59	32	0
	7	S-LAL10	32	0
	8		32	0
	9	S-LAH52	32	0
	10		32	0
	11		23.93795	0
	12		—	—
	13		—	—
	14	MIRROR	58.03327	10
	15		—	—
	16		—	—
	17	LAK9	56	0
	18		56	0
	19	BK7	48	0
	20		48	0
	21	ZKN7	12.26971	0
	22		13.15502	0
	IMA		13.37684	0
	40	Surface OBJ	STANDARD	
		Scattering	None	
	40	Surface STO	STANDARD	
		Scattering	None	
	40	Surface 2	STANDARD	
		Scattering	None	
	45	Surface 3	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	12	
		Scattering	None	
	50	Surface 4	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	12	
		Scattering	None	
	50	Surface 5	STANDARD	
		Aperture	Circular Aperture	
		Minimum Radius	0	
		Maximum Radius	12.7	
		Scattering	None	
	55	Surface 6	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	16	
		Scattering	None	
	60	Surface 7	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	16	
		Scattering	None	
	60	Surface 8	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	16	
		Scattering	None	
	65	Surface 9	STANDARD	
		Aperture	Floating Aperture	
		Maximum Radius	16	
		Scattering	None	

TABLE 1-continued

TABLE 1-continued

LENS DATA		LENS DATA					
Surface 9	STANDARD	5	COATING DEFINITIONS: GLOBAL VERTEX COORDINATES, ORIENTATIONS, AND ROTATION/OFFSET MATRICES: Reference Surface: 2				
Aperture	Floating Aperture						
Maximum Radius	16						
Scattering	None						
Surface 10	STANDARD	10	R11	R12	R13	X	
Aperture	Floating Aperture		R21	R22	R23	Y	
Maximum Radius	16		Surf	R31	R32	R33	Z
Scattering	None		0	1.000000	0.000000	0.000000	0.000000
Surface 11	STANDARD			0.000000	1.000000	0.000000	0.000000
Scattering	None			0.000000	0.000000	1.000000	0.000000
Surface 12	COORDBRK	15	1	1.000000	0.000000	0.000000	0.000000
Decenter X	0			0.000000	1.000000	0.000000	0.000000
Decenter Y	0			0.000000	0.000000	1.000000	-3000.000000
Tilt About X	35		2	1.000000	0.000000	0.000000	0.000000
Tilt About Y	0			0.000000	1.000000	0.000000	0.000000
Tilt About Z	0			0.000000	0.000000	1.000000	0.000000
Order	Decenter then tilt	20	3	1.000000	0.000000	0.000000	0.000000
Scattering	None			0.000000	1.000000	0.000000	0.000000
Surface 13	COORDBRK		4	0.000000	0.000000	1.000000	9.000000
Decenter X	0			1.000000	0.000000	0.000000	0.000000
Decenter Y	-14.704516			0.000000	1.000000	0.000000	0.000000
Tilt About X	0		5	0.000000	0.000000	1.000000	16.000000
Tilt About Y	0	25		1.000000	0.000000	0.000000	0.000000
Tilt About Z	0			0.000000	1.000000	0.000000	0.000000
Order	Decenter then tilt		6	0.000000	0.000000	1.000000	24.000000
Scattering	None			1.000000	0.000000	0.000000	0.000000
Surface 14	STANDARD		7	0.000000	0.000000	1.000000	24.467447
Scattering	None	30		1.000000	0.000000	0.000000	0.000000
Surface 15	COORDBRK			0.000000	0.000000	1.000000	30.467447
Decenter X	0		8	1.000000	0.000000	0.000000	0.000000
Decenter Y	-0.7545004			0.000000	1.000000	0.000000	0.000000
Tilt About X	0		9	0.000000	0.000000	1.000000	42.467447
Tilt About Y	0			1.000000	0.000000	0.000000	0.000000
Tilt About Z	0	35		0.000000	1.000000	0.000000	0.000000
Order	Decenter then tilt		10	0.000000	0.000000	1.000000	43.467447
Scattering	None			1.000000	0.000000	0.000000	0.000000
Surface 16	COORDBRK		11	0.000000	0.000000	1.000000	51.467447
Decenter X	0			1.000000	0.000000	0.000000	0.000000
Decenter Y	0	40		0.000000	1.000000	0.000000	0.000000
Tilt About X	23			0.000000	0.000000	1.000000	53.381402
Tilt About Y	0		12	1.000000	0.000000	0.000000	0.000000
Tilt About Z	0			0.000000	0.819152	-0.573576	0.000000
Order	Decenter then tilt			0.000000	0.573576	0.819152	100.381402
Scattering	None		13	1.000000	0.000000	0.000000	0.000000
Surface 17	STANDARD	45		0.000000	0.819152	-0.573576	-12.045234
Aperture	Circular Aperture			0.000000	0.573576	0.819152	91.947238
Minimum Radius	0		14	1.000000	0.000000	0.000000	0.000000
Maximum Radius	28			0.000000	0.819152	-0.573576	-12.045234
Scattering	None			0.000000	0.573576	0.819152	91.947238
Surface 18	STANDARD	50	15	1.000000	0.000000	0.000000	0.000000
Aperture	Floating Aperture			0.000000	0.819152	-0.573576	-24.134814
Maximum Radius	28			0.000000	0.573576	0.819152	107.897515
Scattering	None		16	1.000000	0.000000	0.000000	0.000000
Surface 19	STANDARD			0.000000	0.529919	-0.848048	-24.134814
Aperture	Floating Aperture			0.000000	0.848048	0.529919	107.897515
Maximum Radius	24	55	17	1.000000	0.000000	0.000000	0.000000
Scattering	None			0.000000	0.529919	-0.848048	18.267591
Surface 20	STANDARD			0.000000	0.848048	0.529919	81.401552
Aperture	Floating Aperture		18	1.000000	0.000000	0.000000	0.000000
Maximum Radius	24			0.000000	0.529919	-0.848048	25.051976
Scattering	None			0.000000	0.848048	0.529919	77.162198
Surface 21	STANDARD	60	19	1.000000	0.000000	0.000000	0.000000
Scattering	None			0.000000	0.529919	-0.848048	26.748072
Surface 22	STANDARD			0.000000	0.848048	0.529919	76.102360
Scattering	None		20	1.000000	0.000000	0.000000	0.000000
Surface IMA	STANDARD	65	21	1.000000	0.000000	0.000000	57.532218
Scattering	None			0.000000	0.848048	0.529919	56.866290
				0.000000	0.529919	-0.848048	60.924410
				0.000000	0.848048	0.529919	54.746613

TABLE 1-continued

LENS DATA				
22	1.000000	0.000000	0.000000	0.000000
	0.000000	0.529919	-0.848048	63.536399
	0.000000	0.848048	0.529919	53.114462
23	1.000000	0.000000	0.000000	0.000000
	0.000000	0.529919	-0.848048	63.960423
	0.000000	0.848048	0.529919	52.849502

What is claimed is:

1. A display system comprising:

- a light source for producing a beam of white light along a path;
- a sequential color filter receiving said beam of white light to form a filtered beam of light having a first cross section;
- a spatial light modulator having a second cross section; distortion optics on an optical path between said sequential color filter and said spatial light modulator, said distortion optics operable to receive and distort said filtered beam to a filtered beam having a cross section more efficiently coupled to said spatial light modulator than said first cross section; and
- a controller electrically connected to said spatial light modulator for providing image data to said spatial light modulator, said spatial light modulator operable to modulate said filtered beam according to said image data.

2. The display system of claim 1, comprising:

- a recycling integrator on said path of said white light beam.

3. The display system of claim 1, comprising:

- a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section.

4. The display system of claim 1, comprising:

- a recycling integrator on said path of said white light beam, said recycling integrator having a reflective exit face with an aperture defining said first cross section.

5. The display system of claim 1, said sequential color filter comprising:

- a spiral color wheel.

6. The display system of claim 1, comprising:

- a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section; and
- said sequential color filter comprising a spiral color wheel, said first cross section having at least one curved side following a boundary between two segments on said spiral color wheel.

7. The display system of claim 6, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters.

8. The display system of claim 6, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters across their entire width.

9. The display system of claim 6, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters and at least one clear filter.

10. The display system of claim 6, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters across their entire width and at least one clear filter across its width.

11. The display system of claim 1, said distortion optics comprising:

- a spherical mirror.

12. The display system of claim 1, said distortion optics comprising:

- an aspherical mirror.

13. The display system of claim 1, said distortion optics comprising:

- a spherical lens.

14. The display system of claim 1, said distortion optics comprising:

- an aspherical lens.

15. The display system of claim 1, said distortion optics comprising:

- a mirror and lens.

16. The display system of claim 1, said distortion optics distorting a curved image of a boundary between two adjacent filter segments to align with rows of said spatial light modulator such that said distorted image of said boundary is imaged across less of said rows than said undistorted boundary image.

17. A method of illuminating a spatial light modulator, the method comprising:

- producing a beam of white light along a path;
- sequentially color filtering said beam of white light to form a filtered beam of light having a first cross section;
- distorting said filtered beam of light to have a second cross section; and
- spatially modulating said distorted beam of light using a spatial light modulator, said distorting operable to improve the alignment of filter boundaries to groups of spatial light modular elements.

18. The method of claim 17, comprising:

- recycling light rejected by said sequentially color filtering.

19. The method of claim 17, comprising:

- recycling light rejected by said sequentially color filtering using a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section.

20. The method of claim 17, comprising:

- recycling light rejected by said sequentially color filtering using a recycling integrator on said path of said white light beam, said recycling integrator having a reflective exit aperture defining said first cross section.

21. The method of claim 17, said sequentially color filtering comprising:

- sequentially color filtering said beam of white light to using a spiral color wheel to form a filtered beam of light having a first cross section.

22. The method of claim 17, comprising:

- recycling light rejected by said sequentially color filtering using a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section; and

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said sequentially color filtering comprising sequentially color filtering said beam of white light to using a spiral color wheel, said first cross section having at least one curved side following a boundary between two segments on said spiral color wheel.

23. The method of claim 22, said recycling light comprising:

recycling light rejected by said sequentially color filtering using a recycling integrator having an exit aperture with at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters.

24. The method of claim 22, said recycling light comprising:

recycling light rejected by said sequentially color filtering using a recycling integrator having an exit aperture with at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters across their entire width.

25. The method of claim 22, said recycling light comprising:

recycling light rejected by said sequentially color filtering using a recycling integrator having an exit aperture with at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters and at least one clear filter.

26. The method of claim 22, said recycling light comprising:

recycling light rejected by said sequentially color filtering using a recycling integrator having an exit aperture with at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters across their entire width and at least one clear filter across its width.

27. The method of claim 17, said distorting comprising: distorting said filtered beam of light to have a second cross section using a spherical mirror.

28. The method of claim 17, said distorting comprising: distorting said filtered beam of light to have a second cross section using an aspherical mirror.

29. The method of claim 17, said distorting comprising: distorting said filtered beam of light to have a second cross section using a spherical lens.

30. The method of claim 17, said distorting comprising: distorting said filtered beam of light to have a second cross section using an aspherical lens.

31. The method of claim 17, said distorting comprising: distorting said filtered beam of light to have a second cross section using a mirror and lens.

32. The method of claim 17, said distorting comprising: distorting a curved image of a boundary between two adjacent filter segments to align with rows of said spatial light modulator such that said distorted image of said boundary is imaged across less of said rows than said undistorted boundary image.

33. The method of claim 17, comprising: modulating said distorted beam of light using said spatial light modulator.

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34. The method of claim 17, comprising:

modulating said distorted beam of light using said spatial light modulator; and

focusing said modulated light onto an image plane.

35. A display system comprising:

a light source for producing a beam of white light along a path;

a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section; and

a sequential color filter receiving said beam of white light to form a filtered beam of light having a first cross section, said first cross section having at least one curved side following a boundary between two segments on said sequential color filter;

a spatial light modulator having a second cross section; distortion optics on an optical path between said sequential color filter and said spatial light modulator, said distortion optics operable to receive and distort said filtered beam to a filtered beam having a cross section more efficiently coupled to said spatial light modulator than said first cross section.

36. The display system of claim 35, comprising:

a controller electrically connected to said spatial light modulator for providing image data to said spatial light modulator, said spatial light modulator operable to modulate said filtered beam according to said image data.

37. The display system of claim 35, comprising:

a recycling integrator on said path of said white light beam.

38. The display system of claim 35, comprising:

a recycling integrator on said path of said white light beam, said recycling integrator having an exit aperture defining said first cross section.

39. The display system of claim 35, comprising:

a recycling integrator on said path of said white light beam, said recycling integrator having a reflective exit face with an aperture defining said first cross section.

40. The display system of claim 35, said sequential color filter comprising:

a spiral color wheel.

41. The display system of claim 35, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters.

42. The display system of claim 35, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three color filters across their entire width.

43. The display system of claim 35, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters and at least one clear filter.

44. The display system of claim 35, said exit aperture having at least two opposite sides shaped to follow said boundary between two segments on said spiral color wheel, said exit aperture sized to allow said white light beam to illuminate at least three primary color filters across their entire width and at least one clear filter across its width.

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45. The display system of claim 35, said distortion optics comprising:

a spherical mirror.

46. The display system of claim 35, said distortion optics comprising:

an aspherical mirror.

47. The display system of claim 35, said distortion optics comprising:

a spherical lens.

48. The display system of claim 35, said distortion optics comprising:

an aspherical lens.

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49. The display system of claim 35, said distortion optics comprising:

a mirror and lens.

5 50. The display system of claim 35, said distortion optics
distorting a curved image of a boundary between two
adjacent filter segments to align with rows of said spatial
light modulator such that said distorted image of said
10 boundary is imaged across less of said rows than said
undistorted boundary image.

* * * * *